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DATA FOR STANDARD CURVE CHORD STEEL ROOF TRUSSES

By

William Hewitt Bush

A

THESIS

submitted to the faculty of the SCHOOL OF MINES AND METALLURGY OF THE UNIVERSITY OF WISSOURI in partial fulfillment of the work required for the

DEGREE OF

CIVIL ENGINEER

Rolla, Missouri

1930

Approved by .

Prof. of Civil Engineering.

* ACKNOWLEDGMENT *

The truss layout, chart and tables were compiled for the Atlas Iron Works, St. Louis, Missouri by the writer and are presented to the Department of Civil Engineering, Missouri School of Mines and Metallurgy, Rolla, Missouri in the form of a Thesis for the Degree of Civil Engineer, by permission of the Company.

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* * *

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Drawing Number 1.

Standard curve chord steel roof truss design, layout and calculations for shop detailing.

Drawing Number 2.

Weights for curve chord steel roof trusses for different roof loadings and span lengths of 25'-0" to 100'-0".

Drawing Number 3.

Graphic chart for determining the allowable stress of two steel structural angles for different roof loading.

Drawing Number 4.

Table for the size of chord angles for different truss spans; 16'-0" bays, 45#/sq.ft. total roof load.

Drawing Number 5.

Table for the size of chord angles for different truss spans; 20'-0" bays, 45#/sq.ft. total roof load.

Drawing Number 6.

Table for the size of chord angles for different truss spans; 16'-0" bays, 60#/sq.ft. total roof load.

Drawing Number 7.

Table for the size of chord angles for different truss spans; 20'-0" bays, 60#/sq.ft. total roof load.

* TRUSS DESIGN *

In the past the Engineering Department of the structural steel company, by which the writer is employed, has been troubled with having to make a large number of preliminary steel truss designs for the purpose of estimating weights for competitive bids on structural steel building contracts. In order to eliminate this expenditure of time, a study was made of the possibility of making a standard design for curved chord steel roof trusses that would give the desired information by observation.

To making this design the necessary factors to be considered are the change of chord members for the varying roof loading and spans. The chord members would change in size for the different spans but the web members, having very little or no stress, would remain of the same section for all span lengths.

A constant for the radius should be determined, in order to take care of the changing of the span lengths, so that all truss dimensions, when reduced, would be proportional. By taking a truss

of a 100'-0" span, center to center of bearing, for the key truss, all dimensions for the shorter spans will then be directly proportional to the dimensions of the key truss.

In determining the radius for the key truss, the approximate bending moment of the truss would be calculated for a total roof load of 45#/sq.ft., trusses spaced for 16'-0" bays, that is, the bending moment is equal to the total truss load times the length of the span, center to center of bearing, divided by the constant 8; then the chord stress is equal to the bending moment divided by the desired depth of the truss at the center. The actual depth of the truss at the center is obtained by trial depths until the resulting compression chord stress requires the use of economical sections which are carried in stock or are obtainable when desired.

The most economical center of span depth, determined from the approximate method, is found to be about 12'-0". The depth of the truss now known, the radius is found by simple trigonometry. The radius for that depth of truss would be approximately 110'-0", or 1.1 the length of the span. The 1.1 of the span

length for the radius is used for all length of truss spans. The most desirable panel spacing for a 100'-0" truss is ten panels. In checking back for the fibre stress in the compression chord angles, on a 10'-0" span, the angles would be subject to an eccentric moment due to the curve of the top chord, a bending moment due to the roof load and the chord stress. For the key truss this fibre stress is about 10700#/sq.in., where the allowable stress is 14800#/sq.in., taken from the A.I.S.C. compression formula.

The truss layout, shown on Drawing Number 1, shows a curved chord steel roof truss design that is worked out as the standard truss design on the basis of a radius of 1.1 the span length. The stress diagram gives negligible stress for all the web members; the smallest size structural shape is used for all spans or 1-L $2\frac{1}{2}$ "x $2\frac{1}{2}$ "x $\frac{1}{4}$ ". These angles are crossed in each panel to shorten the unsupported length so as to take care of any compression stress that might be applied, due to eccentric loading of the truss; also this condition is to eliminate the use of vertical web angles at the panel points.

In order to determine the compression chord

angles for the different spans, a plot of the most used roof loadings against the allowable stress for the chord angles is shown on the graphic chart, Drawing Number 3. The compression chord stresses, unsupported length of angles and the maximum span that the chord angles should be used for, as determined from the graphic Drawing Number 3, are compiled in tables, Drawing Numbers 4, 5, 6 & 7.

The chord angles to be used for any truss span can readily be obtained by referring to the column headed "Angles for Span". The stresses in the compression chord angles, for any span, with any loading, can be obtained by proportional reduction from the key truss.

* TRUSS WHIGHTS *

In order to reach a close approximation of the weight for trusses of any span length, the truss members should be separated into constant sizes, proportional sizes and variable sizes of members and fittings. These divisions were made as follows:

Constant members:

web rivets web plates anchor bolts

Proportional members:

web angles splice plates end plates bearing plates stitch rivets wood bolts

Variable members:

com. chord angles ten. chord angles

The size of the detail members and fittings of the truss, such as rivet quantities and plate dimensions, were determined by making a large scale drawing of a 100'-0" truss. The total weight for a 100'-0" truss was computed for each loading. In reducing the span lengths by one foot, the constant would carry on, the proportional would reduce one percent and the variable, or the chord angles, would reduce on account of the reduced length, in all

cases, and for size of members where the span length requires the reduction in size of angles. By following this procedure, satisfactory approximate weights were obtained for all interval span lengths of one foot, from 25'-0" to 100'-0". The weights were figured for the most used roof loadings and building bay spacing. These weights are given in table on Drawing Number 2.

If it is desired to find the weight of a truss, that the condition of loading or bay spacing is different, the approximate weight can be obtained by interpolation.

* STRUCTURAL DETAILING *

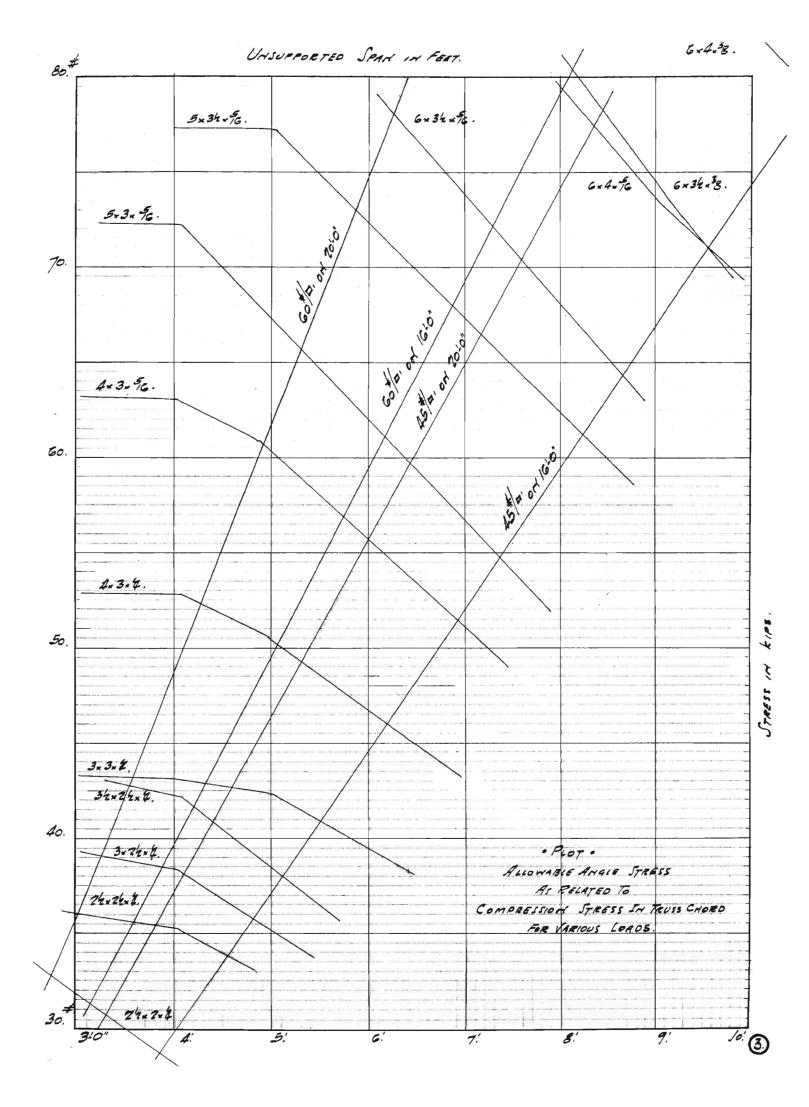
It is necessary to determine all panel and diagonal dimensions for curved chord steel roof trusses for making shop details. These dimensions can be obtained for any truss span by taking the percentage of the desired truss span length of the key truss dimensions. For example: with a desired truss span length of 82'-9", the dimensions would be 82.75% of the dimensions for the key truss, since all dimensions reduce directly porportional to the span length. The stresses in all members are reduced by the same procedure. It is obvious that many hours of time can be saved by this method of calculation.

* CONCLUSION *

The standard curved chord steel roof truss design, proportional dimensions and the table of weights for the most frequently used type of truss for garages, small theatre buildings, one story ware-houses, airplane hangars and factory buildings; will undoubtedly prove invaluable as a time saver both for the Engineering and Estimating Department.

* * *

		WEIC	HT	OF S	TAMO	ARD	CUR	IE C	HORE	Tel	ļss es	25	5-0" TO	100:00	SPAR	45 .	
SPAH.	16'0' BAY.	20-0 BAY 45*/0	160 BAY.	20:0'BAY	APP.MID. Ta,Haigth.	SPAK.	16:0" BAY 45 4	20:0° BAY 45*/=	16:0'BAY.	20:0 BAY	APR MID, TR. HARTH.	SPAN.	16:0 BAY. 45 /2	20:0'BAY. 45*/21	16:0'BAY 60*/0'	20:0'BAY	
75:0"				10 34	3: 3°	51-0"	1723	2/54	2768	2521	6:5"	76-0"	3336	4134	4297	5048	916
26:0"	A CONTRACTOR OF THE CONTRACTOR			10 37	3:4"	52:0"	1751	2191	2307	76 59	6-7"	77:0"	3376	4184		5/10	9:7
27:0			5 6 8 8	1117	3-5"	530"	17.79	2227	2345	2714	6-8"	78:0"	3416	4135	4402	5168	9:8
28-0"				1147	3-7'	54-0	1950	2264	2447	2769	6-10	79:0"	3456	4285	46 32	5230	9:10
29-0"				1201	3:8"	55:0	1980	2300	2487	2931	6:11"	80:0"	3687	4336	4687	5292	9:11
30:0"	1005	10 38	1110	12.55	310"	56:0"	2011	2337	2540	2918	7:1"	81:0"	3729	4386	4741	5354	10:1
31:00	1029	1091	1195	1286	3411"	57:0"	2041	2373	2580	3152	7-2"	82:0"	3761	4537	4796	5416	10:2
32:0"	10.52	1117	1724	1344	4:1"	58:0"	2072	2620	2620	3202	7-4"	83:0"	3803	4589	4850	6234	10:4
33-0"	1075	1142	1253	1404	4:2"	59:0"	2/02	2660	26.59	3252	7:5'	84.0"	4287	4786	4905	6305	10:3
34'0"	1100	1201	1282	1499	4:4"	60:0"	2416	2700	2895	35 40	7:6	85:0"	4354	4779	5159	6376	10:7
350	1/23	1278	1338	1534	4:5"	61:0"	7451	2740	2938	3594	728"	86:0"	4381	4832	5204	6447	1018
36:0	1146	1254	1400	1569	417"	62-0"	2486	2855	2981	36 48	7410"	87-0"	4429	4884	56/3	6518	10:9
37:0'	1206	1312	1429	1672	4-8"	63:0	2522	2896	3059	3702	7411"	88:0"	4476	4937	5674	6589	10:11
38:0"	1231	1340	1489	1708	4:10"	64.0"	25.57	2938	3102	3818	8:0"	89:0"	4523	4990	5735	6427	11:0
39-0"	1255	1423	1520	1745	4411"	650"	2592	2979	3/46	3873	8:2"	90:0"	4743	56/3.	2796	6496	11:2
40:0"	1280	1452	1551	1781	5:1"	66:0"	2627	30 20	3190	3928	8131	91:0"	47 92	5672	5857	6565	11:3
41:0"	1304	1481	1691	1938	5:2"	67-0"	2800	31 32	35 67	3983	8:5"	92:0"	4964	5731	5918	6634	11:5
42:0"	1370	1518	1725	1977	5:4"	68-0"	2838	3/74	3616	4038	8:5"	93:0"	5013	5790	5979	6703	11:6
43'0"	1395	1547	1758	2016	516"	69:0"	2875	3371	3664	1298	8:7"	94:0"	5063	5849	60 40	6772	1128
44.0"	1456	1690	1792	2/28	517"	70:0"	2912	.3416	37/3	4356	8:9"	95:0"	5/12	5998	6481	6841	11: 9
45-0"	1482	1722	1909	2169	5:9"	71:0"	2949	3460	4035	4414	8:10"	96:0"	5/62	5967	6639	6910	11:10
46:0"	1508	1754	1944	2210	5:10	72:0"	3/76	3932	4087	4472	9:00	97:0	5211	6026	6705	7348	12:0
47:0"	1611	1786	1980	23 49	6:0"	73-0"	3216	3982	4140	4530	9:1"	98:0"	5261	6466	6771	7420	124/1
18:0"	1639	1907	2015	23 98	6:1"	74:0"	3756	40 33	4192	4588	9:3"	99:0"	5310	6529	6837	7493	1713
49-0"	15.67	1940	2191	24 35	613"	75:0"	3296	4088	4245	4646	9:4"	100:0"	5360	6592.	6903	8026	12.4
50:0"	1695	1974	22 29	2478	6:4"		1					101:0	5410				
		1					1					107:00	5460				



			CHO	DRO MEM	BERS.			
-	16:0"	BAY	45*/	MAX STRES T. = 73.4#	55 100:0" C.= 77			
SPAH.	UNSUP.	ALLOWADLE ITRESS	CHORD STRESS	COMPRESSION. CHORD	AHOLOS FOR SPAH.	TENSION CHORD	STRESS	SPAM.
102.0	10.58	78.8	78.5	26-6-4-3	100	26-5×3×5	76.58	104.3
91.9	9.52	70.8	70.8	6-34-38	84	4×3×76	65.47	89.1
91.8	9.51	70.7	70.6	6 * 4 * 76	- 80 12	4.4.4	61.30	83,4
79.1	8.20	61.0	61.0	5,32,76	67	4. 3. 7	52.30	71.2
66.6	6.90	جي ربي	51.3	4.3.16	4	3.3.4	43.96	59.8
<i>-59.0'</i>	5.11	45.5	45.5	4.3.4	47	3.24.4	39.28	53.5
52.6	5.45	40.6	40.6	3-3-8	-4 7	24.24.4	34.9C	46.9
46.1	4.77	35.7	35.7	3, 24 - 4	12	22×2×4	30.26	41.2
43.2	4.48	33.5	33.5	24-24-2	37			
36.7	3.80'	28.7	28.7	24-2×4	1			



			CHO	DRO MEM	BER5	•		
	20	0" BAY	Max Stress 10010" Span T = 91.7" C = 92.2"					
SPAH.	UNSUP. PORTED	ALLOWARIE STRESS	CHORO STRESS	COMPRESSION CHORD	AMQLES FOR SPACE	TEMSION CHORD	ALLOWARIE STRESS	SPAM
104.3'	10.81	100.9	100.6	26-6×4×2	100'	21s 6× 4× 96	107.2	98.4
97.0'	10.06	94.4	93.5	T = 4= 76	97	6 * 3 2 * 76	101.1	92.8
89.7'	9.30	86.2	86.3	6×4×38	89	5×31×56	89.8	82.3
81.0'	8,40'	78.2	18.2	6-32-38	81	5×3×56	83.5	76.2
12.9'	7.50	70.2	10.2	6×32×5	68	4 3 = 16	71.3	65.4
68.8'	7.13'	66.3	66.3	5 x 3 2 x , 5	66	4.4.4	66.9	5/
61.7	6.40	59.5	59.5	5 + 3 + 76	37 -7	4.3.2	57.0	57.3
57.Z'	5.93	55.3	55.3	4-3-76	50	3-3-4	47.9	43.9
50.6	5.75	49.0	49.0	4.3.4	43	3-22-2	42.9	39.3
43.9'	4.55	42.5	42.5	3 - 3 - 4	31	22-22-4	38.1	34.9
41.9	4.34	40.6	40.6	32-22-4	38 56	24 2 * 4	33.0	30.3
39.0'	4.04	37.9	37.9	3×24×4	33 30			
36.1'	3.74	35.2	35.2	24 × 24 × 4	7			

	164	O" BAY	MAX STRE T. = 97.8#	55 100-0° C.= 102.				
SPAH.		ALLOWABLE STRESS	CHORD STRESS	COMPRESSION CHORD	ANGLUS FOR SPAN.	TENSION CHORD	ANGLE STRESS	SPAM
100.0'	10.37'	104.0	102.7	215-6-4-12	98	7Ls:- 6× 4× 5c	100,5	98.4
94.0'	9.75'	96.7	96.5	6×4×1c	94 86	6×34×56	95.0	92.6
86.0	8.97	88.5	88.7	6×4×3	. 84	5 x 3 2 x 5 C	84.1	82.
78.0'	8.10	80.5	80.5	6x 32x 3	78	5×3×96	78.3	76.0
70.1	7.27	12.0	72.0	6x 32x 48	æ	4 3 4 96	66.8	65
66.0'	6.85	67.7	67.7	5x 3/cx 76	59	4.4.4	62.7	61.
59.5'	6.18'	61.0	61,0	5x 3 x 96	53	4.3.4	53.5	52.
55./	5.72	56.5	56.5	4× 3× 96	48	3x 3x 4	44.9	43.
48.G'	5.05	49.9	49.9	4n3x4	1	3-22-4	40.1	39.
41.6'	4.32'	42.5	47.6	3 × 3 × 4	31/1	22.22.4	35.7	34.
40.5	4.20'	41.3	41.3	34 2 2 2 4	35	24.2.4	30.9	30.
37.3'	3.87	38.0	38.0	3. 22. 4	10			
34.7'	3.60	35.3	<i>35.</i> 3	27 = 27 = 2	11			
30.8	3.70	31.4.	31.4.	22 2 2 2	}			

	, loo's SPAN,							
	20-	O" BAY	C.= 128.	3.4 =				
SPAH.	Um sup. PORTED	ALLOWABLE STRESS	CHORD STRESS	COMPERSSION CHORD	ANGLES FOR SPANS	TENSION CHORO	ANGLE STRESS	SPAN
100.0'				215-6-6-76	100'	218-6-4-76	136.7	111.
99.0'	10.25	126.7	127.0	6×6×38	88	6×4×38	118.2	96.0
88.0'	9.14	1/3.8	1/3.0	6 * 4 * 2	82	6 * 4 * 76	100.5	87.
82.0	8.52	105.2	105.5	6 . 4 . 76	77	6 + 3 2 + 7 E	95.0	77
75.0'	7.78	96.3	96.3	6.4.3	68	5.32.5	84.1	68.
68.0	7.07	87.5	87.3	6.32.3	53 59	5, 3, 5	78.3	63.
59.9	6.22	77.9	77.9	6.32.6	56	4.3.16	66.8	54.
56.1	5.83	72.8	72.8	5. 32.76	51	4.4.4	62.7	51.
50.8	5.28	65.6	E5.6	5 * 3 * 76	43	4.3.8	53.5	43.
46.9'	4.87	60.3	60.3	4-3-56	36	3.3.5	44.9	36.
40.7'	4.23	51.9	51.9	4, 3, 4	33	3.22.4	40.1	32.
<i>33.7</i> '	3.50	42.5	47.5	32-24-4	31	22.22.4	35.7	29.
31.0'	3.72	38.8	38.8	3-24-4	28 25	22-2-4	30.9	25.