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Summary Report: Strength of Single L-headers

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research report

Summary Report: Strength of Single L-Headers

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PREFACE

This report summarizes a previous test program conducted at the NAHB Research Center, and proposes a design methodology for single L-headers under gravity load. The findings provided a basis for the AISI Committee on Framing Standards to establish design options for single L-headers in the AISI *Standard for Cold-Formed Steel Framing – Header Design*.

Research Team
Steel Framing Alliance

Summary Report
Strength of Single L-Headers
R. A. LaBoube
January 30, 2004

Introduction

Based on a test program performed at the NAHB Research Center (NAHB, 2003), a design methodology is proposed for single L-headers under gravity load. This report briefly summarizes the NAHB test program and presents justification for a proposed design method.

NAHB Test Program

The test specimens were single span assemblies consisting of the top and bottom track, cripple stud, and simulated wall stud. A single L-header was affixed to the top track as illustrated by Figure 1.

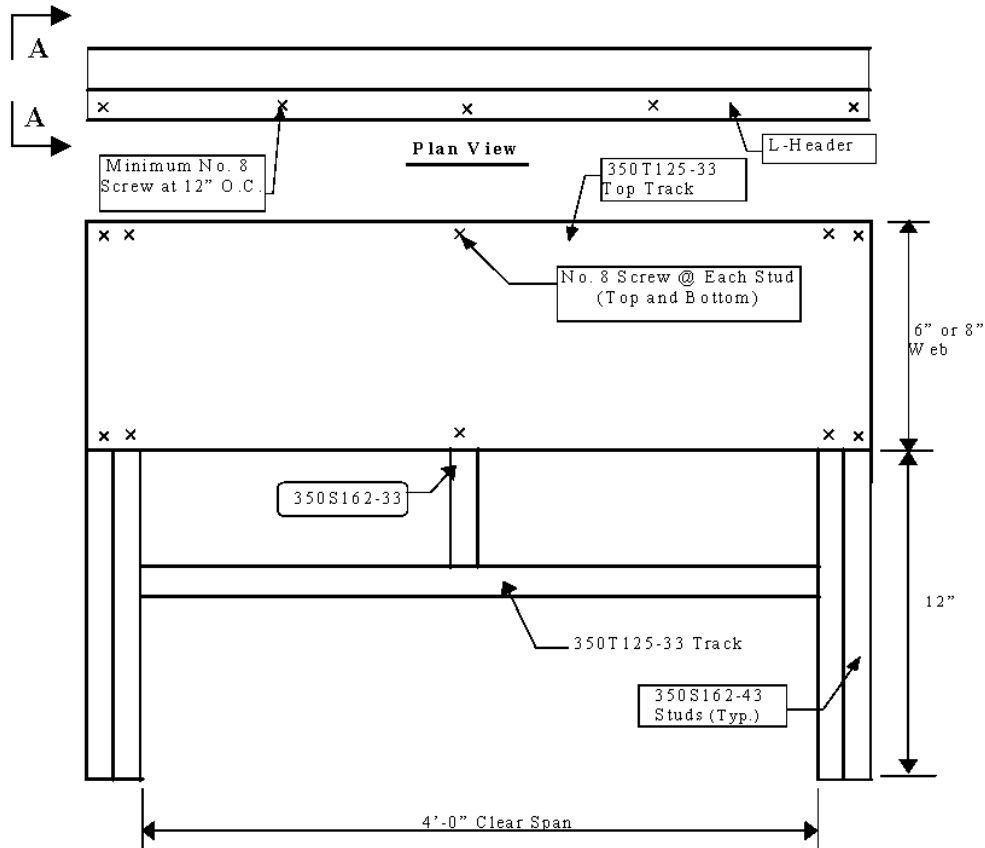


Figure 1 Single L-Header Test Assembly

Using No. 8 self-drilling screws, the L-header was screw attached to both the top track and to each stud as depicted by Figure 1 and Figure 2. Except that only a single L-header was installed, the construction of the tested assemblies met the installation requirements of the Header Standard (AISI, 2001), per Figure A1.1.2 for double L-headers.

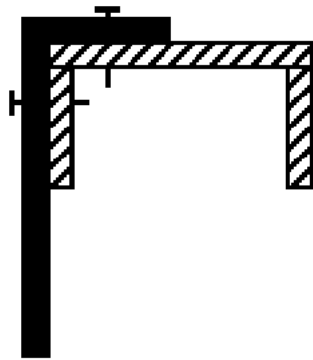


Figure 2 Typical L-Header Attachment to Track

To simulate in-situ loading of the header, each single span assembly was subjected to concentrated load at the mid-span cripple stud (Figure 3). Each assembly was tested to failure.

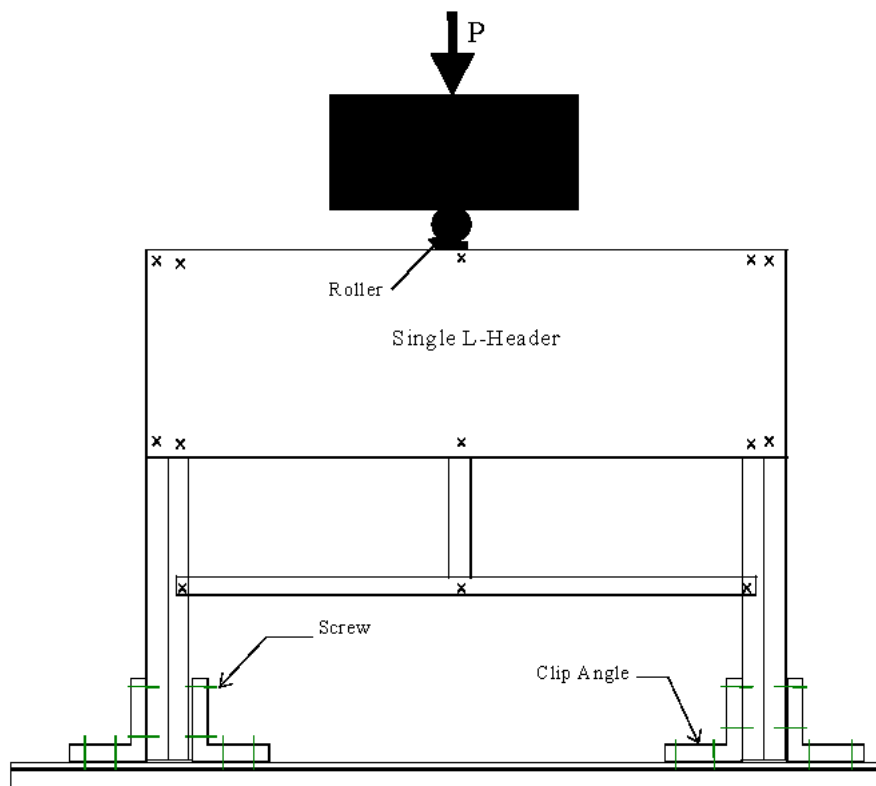


Figure 3 Load Application

Evaluation of Test Data

A total of 18 single L-header assemblies were tested to failure. Material tensile test properties are summarized in Table 1.

Table 1 - Material Tensile Properties for the L-Headers

| L-Header (Angle) Designation | Yield Point ¹ (psi) | Tensile Strength ¹ (psi) | Uncoated Thickness ² (inch) | Elongation ³ (percent) |
|------------------------------|--------------------------------|-------------------------------------|--|-----------------------------------|
| 600L150-33 | 36,800 | 46,100 | 0.0337 | 18.5 |
| 600L150-33 | 38,200 | 45,200 | 0.0341 | 18.7 |
| 600L150-33 | 37,500 | 48,600 | 0.0340 | 19.4 |
| 600L150-43 | 41,100 | 55,300 | 0.0444 | 19.6 |
| 600L150-43 | 39,900 | 54,600 | 0.0451 | 21.2 |
| 600L150-43 | 40,500 | 53,400 | 0.0448 | 20.0 |
| 600L150-54 | 53,700 | 64,600 | 0.0551 | 19.5 |
| 600L150-54 | 52,800 | 67,800 | 0.0555 | 19.9 |
| 600L150-54 | 54,100 | 65,200 | 0.0546 | 21.3 |
| 800L150-33 | 36900 | 48600 | 0.0339 | 23.2 |
| 800L150-33 | 37200 | 45900 | 0.0335 | 22.1 |
| 800L150-33 | 37100 | 46200 | 0.0336 | 20.9 |
| 800L150-43 | 39800 | 56900 | 0.0439 | 22.9 |
| 800L150-43 | 38700 | 58200 | 0.0441 | 21.6 |
| 800L150-43 | 40100 | 55800 | 0.0440 | 19.8 |
| 800L150-54 | 56500 | 69200 | 0.0540 | 21.6 |
| 800L150-54 | 54900 | 67500 | 0.0541 | 19.8 |
| 800L150-54 | 53800 | 68300 | 0.0541 | 22.3 |

For SI: 1 inch = 25.4 mm, 1 psi = 0.0703 kg/cm²

¹Yield point and tensile strength shown are based on coupons cut from each sample and tested per ASTM A370 [6].

²Uncoated thickness shown is based on uncoated thickness taken from each sample per ASTM A90 [7].

³Tested in accordance with ASTM A370 [6] for a two-inch gauge length.

Each assembly was tested as an assumed simple span beam with a concentrated load at mid-span. The test failure load, P_u , and the corresponding simple span moment is given in Table 2,

$$M_{\text{test}} = P_u L / 4 \quad (1)$$

where $L = 48$ inches.

Using the AISI Specification (AISI, 1999), the elastic section modulus of the effective section calculated at $f = F_y$ in the extreme compression fibers, S_{ec} , was computed for each L-header test assembly. Only the single L-header geometry was considered when computing S_{ec} . The nominal moment capacity, M_{ng} , was computed using Eq. B3.1.1-1 from the 2001 Header Standard (AISI, 2001) as

$$M_{ng} = S_{ec} F_y \quad (2)$$

where F_y = yield point as given in Table 1.

Table 2 - Test and Analysis Results

| Section | Fy ksi | Sec in3 | Mng in-kips | Pu kips | Mtest in-kips | Mtest/Mn |
|------------|-----------|------------|----------------|------------|------------------|----------|
| 600L150-33 | 36.8 | 0.285 | 10.49 | 1.87 | 22.44 | 2.140 |
| 600L150-33 | 38.2 | 0.288 | 11.00 | 1.89 | 22.67 | 2.060 |
| 600L150-33 | 37.5 | 0.287 | 10.76 | 1.70 | 20.41 | 1.897 |
| 600L150-43 | 41.1 | 0.398 | 16.36 | 2.02 | 24.22 | 1.480 |
| 600L150-43 | 39.9 | 0.410 | 16.36 | 2.18 | 26.16 | 1.599 |
| 600L150-43 | 40.5 | 0.406 | 16.44 | 2.34 | 28.12 | 1.710 |
| 600L150-54 | 53.7 | 0.509 | 27.33 | 2.81 | 33.74 | 1.235 |
| 600L150-54 | 52.8 | 0.516 | 27.24 | 2.91 | 34.88 | 1.280 |
| 600L150-54 | 54.1 | 0.503 | 27.21 | 2.81 | 33.71 | 1.239 |
| 800L150-33 | 36.9 | 0.400 | 14.76 | 2.19 | 26.28 | 1.780 |
| 800L150-33 | 37.2 | 0.383 | 14.25 | 2.20 | 26.42 | 1.855 |
| 800L150-33 | 37.1 | 0.387 | 14.36 | 2.26 | 27.17 | 1.892 |
| 800L150-43 | 39.8 | 0.642 | 25.55 | 2.81 | 33.72 | 1.320 |
| 800L150-43 | 38.7 | 0.647 | 25.04 | 2.77 | 33.22 | 1.327 |
| 800L150-43 | 40.1 | 0.643 | 25.78 | 2.93 | 35.20 | 1.365 |
| 800L150-54 | 56.5 | 0.797 | 45.03 | 3.19 | 38.26 | 0.850 |
| 800L150-54 | 54.9 | 0.801 | 43.97 | 3.13 | 37.60 | 0.855 |
| 800L150-54 | 53.8 | 0.803 | 43.20 | 3.34 | 40.03 | 0.927 |
| | | | | | Mean | 1.489 |
| | | | | | Std. | |
| | | | | | Dev. | 0.400 |
| | | | | | COV | 0.2689 |

Conclusion

Based on the computed ratios of M_{test}/M_{ng} listed in Table 2, Equation 2 (Eq. B3.1.1-1 from the 2001 Header Standard) is an acceptable relationship for evaluating the gravity moment capacity of the single L-header assemblies tested, except for the 8 inch deep 54-mil L-headers which did not achieve design strength. The design methodology should be adjusted to reflect this observed behavior. Using the provision of Chapter F1 of the AISI specification, $\Omega = 1.67$ and $\phi = 0.90$. These are the same factors prescribed in the 2001 Header Standard (AISI, 2001) for the design of double L-headers.

As with previously tested double L-headers, neither pure shear or combined bending and shear were failure modes in the test program. Also, web crippling and combined bending and web crippling are precluded from occurring because of the requirement that concentrated load applications occur at cripple stud locations.

Recommendation

The 2001 Header Standard (AISI, 2001) should be revised to incorporate single L-headers within the ranges tested.

References

AISI (1999), Specification for the Design of Cold-Formed Steel Structural Members, 1996 Edition with 1999 Supplement, American Iron and Steel Institute, Washington, D.C.

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NAHB (2003), “Testing of Steel Single L-Headers”, U.S. Department of Housing and Urban Development, Washington, D.C.



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