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IMPLEMENTATION OF TI545 IN AIR PRESSURE CONTROL

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ABSTRACT

The Texas Instruments Model 545 programmable logic controller is used to control the air pressure in a heating/ventilation simulator designed and built for a classroom experiment station. Through the use of the PLC's built-in PID algorithm, the pressure in the duct was controlled to within a 2% tolerance and over 72% of the sensor range for a load setting of 10%. The theory of PID controllers and their application to this problem are discussed. Also, the configuration of the simulator, and plans for future work are described.

THEORY

The Proportional-Integral-Derivative (PID) controller, because of its simplicity and effectiveness, is one of the most widely used control schemes in industry. Fundamentally, the PID is a feedback loop with three terms in the feedback transfer function: proportional, integral, and derivative. The proportional term responds to changes in the process variable, but a P controller settles at an offset value that is different from the process set-point. The integral term remedies this problem by responding to the integral of the difference between set-point and process variable values. However, in some circumstances, the integral term can saturate the controller and render it useless. The use of an integral reset coefficient can fix this problem. The derivative term is added in some situations for faster response and better damping characteristics.

SYSTEM DESCRIPTION

The heating/ventilation simulator (see Figure 1) consists of a piece of ordinary air ducting with a 3-phase blower on one end, a heating element inside, and a variable opening on the other end to simulate varying loads on the H/V system. The blower is driven by an Allen Bradley variable-frequency motor drive, with a range of 0.5 to

60 Hertz. The drive frequency is controlled by a 0-10 Volt analog signal from the PLC. An Omega pressure sensor with a range of 0-1" H₂O is located close to the opening and sends a 4-20 mA analog signal to the PLC.

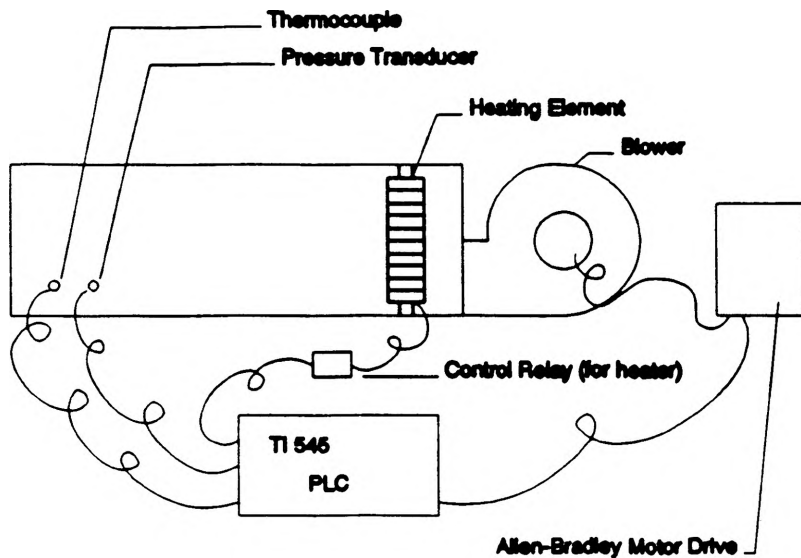


Figure 1

CONTROL

There are three primary parameters which affect the pressure inside the duct: (1) the speed of the blower, (2) the load setting, and (3) the temperature in the duct. To simplify the investigation, the load was considered to be a system disturbance and not controllable by the PLC. Also, the effect of temperature on the pressure was neglected. In essence, the duct air pressure was considered to be a direct function of only the speed of the blower. The block diagram of this simplified system is shown in Figure 2.

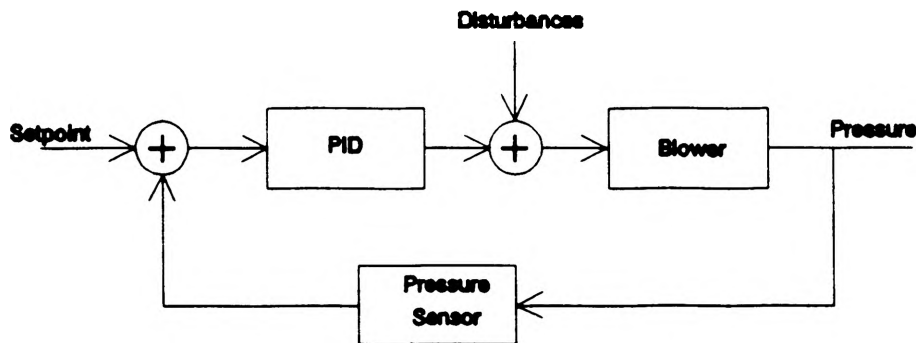


Figure 2

The Laplace transform of the PID loop is given by equation 1.

$$M = K_c (E + E/(T_i s) + CT_d s) + M_x/s \quad (1)$$

Where:

- M = PID loop output
- E = Set point - process variable
- C = Process variable (pressure in duct)
- M_x = Loop output when E = 0
- K_c = Proportional Gain
- T_i = Reset coefficient
- T_d = Derivative coefficient

As was mentioned before, the PLC has a pre-programmed PID algorithm so that the application engineer has only to "fill in the blanks" to set up and tune the controller. The set-point is held in a special dedicated variable called LSPX (where X is the loop number, 1-64.) In this case, the process variable (C) is contained in WX49, which is the address of the analog pressure sensor value after A-D conversion. The parameters K_c, T_i, and T_d are directly entered into the PID loop table (Appendix A.) It was found that values of 0.75, 0.09, and 0, respectively, gave the best performance. T_d was set to zero because taking the derivative of the inherently noisy pressure signal puts wild swings into the loop output. This effectively classifies this control as a PI control rather than a PID.

PERFORMANCE

The PI controller is not aggressively tuned and the settling time equals the rise time. There is no sinusoidal "bouncing" around the set point, so once it is within tolerance, it stays within tolerance. Table 1 shows the 95% rise times when the set point was changed in a step from 10% to another value. For each measurement, the system was allowed to settle at the 10% point before input of the new set-point value. The control was able to hold the process variable to within 1.3% of the set point. In the table, t_r is given in seconds, set-points are given in hundredths of an inch of water (which corresponds to percent of sensor range.)

TABLE 1: RISE TIMES

<u>New Set Point</u>	<u>t_r</u>
15	14
20	22
25	27
30	29
40	29
50	30
60	30
72	30

PROGRAMMING

The basic programming tools of the PLC logic are discrete and analog inputs and outputs, control relays, timers, counters, math special functions, and various bit and word manipulation functions. Most of the programming of this project was accomplished in math special functions. The ladder listing and special function listing are in Appendix A.

The basic operation of the system is to use a selector switch (X3, X4, X5, X6) to choose one of two pressure set-points (or one of two temperature set-points in the future.) Then using momentary push buttons (X7-up,X8-down,) the set point is incremented up or down by one percent. The value is displayed on an LED readout (Y17-Y24.) When the START button (X1) is pressed the value from the display is loaded into LSP1 (the PID algorithm's dedicated set-point address,) the loop is set to automatic mode, and the control relay (Y29) for the frequency drive is turned on. The set point may be changed at any time with no effect on the loop until the START button is pressed. Pressing the STOP button (X2) turns off the freq. drive relay and takes the PID loop out of automatic mode. The two lamps (Y26, Y28) are turned on and off by the control loop flag (C106) which shows the sign of the E in the loop. For example, if the system is stepped to 60 from a value of 20, the Error (set-point - process variable) will be positive until the process variable becomes greater than the set-point. This was handy for tuning, since one could see the system was settled when the two lights began blinking back and forth rapidly.

FUTURE WORK

Plans for future experimentation consist mainly of developing a temperature control loop, a better user interface, and perhaps implementing a fuzzy controller to replace the PID algorithm. All three of these will be totally software changes, as the temperature control hardware is already in place.

The most immediate of these projects will be the temperature control loop. It will be almost identical in structure to the pressure control loop except that the heating element (driven by a relay) is either off or on. There is no analog control of the heating hardware. Therefore a proportional time control scheme will be implemented, where the output from the PID will go to a math function which will calculate a duty cycle for the heating element. One of the issues to be resolved in this problem will be finding the optimum period of the off/on total cycle.

CONCLUSION

By holding the pressure to within 1.3% of the set point, PLC PID controller has proven its viability to an HVAC application. The ease with which the application engineer is able to assemble a working system highlights the flexibility and explains the popularity of the industrial programmable logic controller.

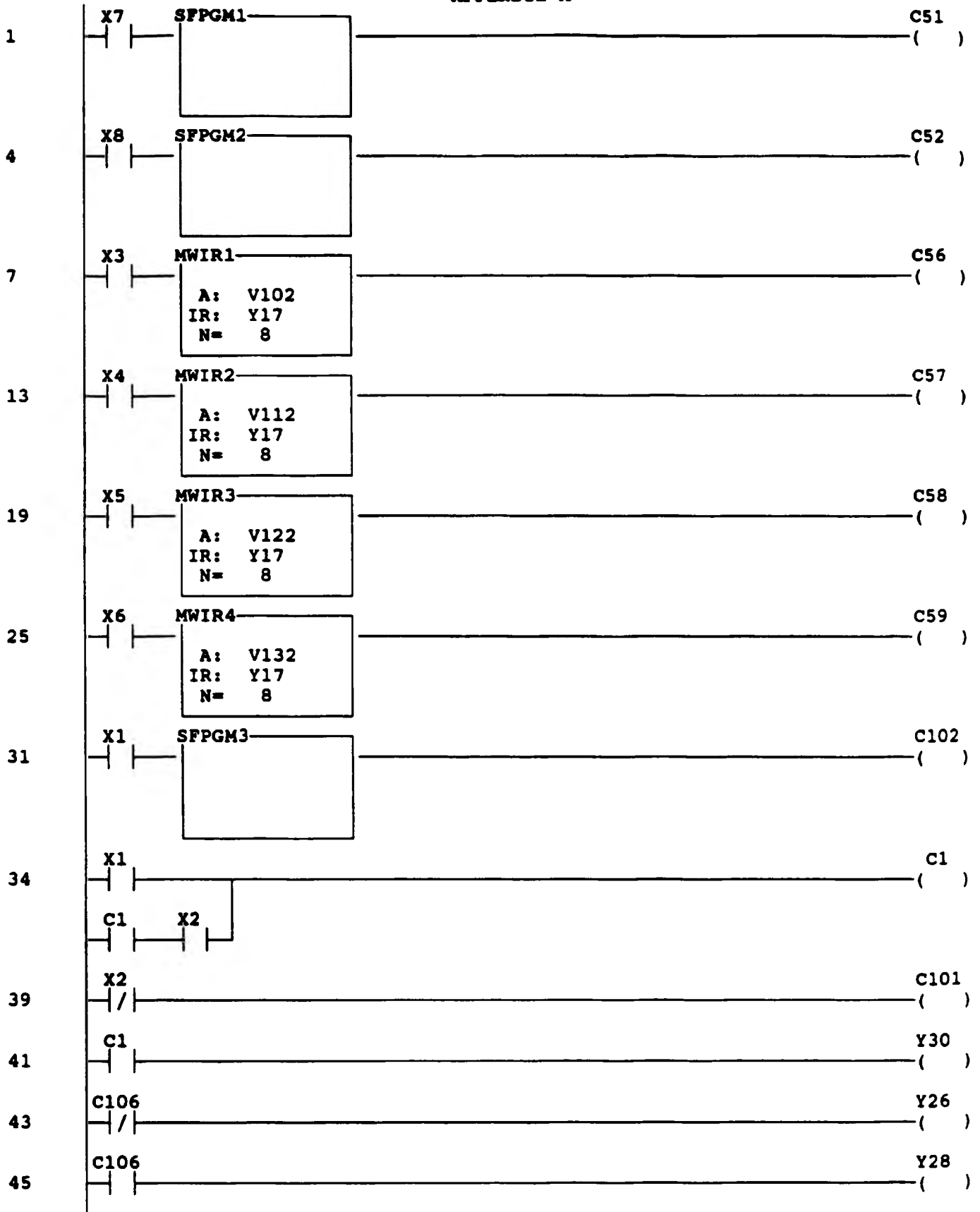
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APPENDIX A



PID LOOP 1 TITLE: PRESSURE
POS/VEL PID ALGORITHM: POS
LOOP VFLAG ADDRESS: C101
SAMPLE RATE (SECS): +0.10000
PROCESS VARIABLE ADDRESS: WX49
PV RANGE: LOW = +20.0000
HIGH = +100.000
PV IS BIPOLAR: NO
SQUARE ROOT OF PV: NO
20% OFFSET ON PV: YES
LOOP OUTPUT ADDRESS: WY57
OUTPUT IS BIPOLAR: NO
20% OFFSET ON OUTPUT: NO
RAMP/SOAK PROGRAMMED: NO
RAMP/SOAK FOR SP: NO
ALARM DEADBAND: +2.00000
MONITOR LOW-LOW/HI-HI: NO
MONITOR LOW/HIGH: NO
PV ALARMS: LOW-LOW = +41.0000
LOW = +45.0000
HIGH = +55.0000
HIGH-HIGH = +59.0000

REMOTE SETPOINT: NONE
CLAMP SP LIMITS: LOW = +20.0000
HIGH = +100.000
LOOP GAIN: +0.75000
RESET (INTEGRAL TIME): +0.09000
RATE (DERIVATIVE TIME): +0.00000
FREEZE BIAS: NO
DERIVATIVE GAIN LIMITING: NO
LIMITING COEFFICIENT: +10.0000
SPECIAL CALCULATION ON: NONE
SPECIAL FUNCTION: NONE
LOCK SETPOINT: NO
LOCK AUTO/MANUAL: NO
LOCK CASCADE: NO
ERROR OPERATION: NONE
REVERSE ACTING: NO
MONITOR DEVIATION: NO
DEVIATION ALARM: YELLOW = +3.00000
ORANGE = +5.00000
MONITOR RATE OF CHANGE: NO
RATE OF CHANGE ALARM: +0.00000
MONITOR BROKEN XMITTER: NO

CONTINUE ON ERROR (Y,N): NO
ERROR STATUS ADDR (Y,C,WY,V): V50 - V52
PROGRAM TYPE (N,P,C,R): PRIORITY
CYCLE TIME (SEC): 0.0

```
00001 *      INCREMENTS HIGH TEMP SET-POINT WITH
              ACTIVATION OF UP/DOWN SWITCHES
00002 IF      X3
00003 MATH    V101 := V101 + 1
00004 ENDIF
00005 IF      V101 > 99
00006 MATH    V101 := 99
00007 ENDIF
00008 BINBCD  BINARY INPUT..: V101          BCD RESULT....: V102
00009 IF      X4
00010 MATH    V111 := V111 + 1
00011 ENDIF
00012 IF      V111 > 99
00013 MATH    V111 := 99
00014 ENDIF
00015 BINBCD  BINARY INPUT..: V111          BCD RESULT....: V112
00016 IF      X5
00017 MATH    V121 := V121 + 1
00018 ENDIF
00019 IF      V121 > 99
00020 MATH    V121 := 99
00021 ENDIF
00022 BINBCD  BINARY INPUT..: V121          BCD RESULT....: V122
00023 IF      X6
00024 MATH    V131 := V131 + 1
00025 ENDIF
00026 IF      V131 > 99
00027 MATH    V131 := 99
00028 ENDIF
00029 BINBCD  BINARY INPUT..: V131          BCD RESULT....: V132
****  END  ****
```

CONTINUE ON ERROR (Y,N): NO
ERROR STATUS ADDR (Y,C,WY,V): V53 - V55
PROGRAM TYPE (N,P,C,R): PRIORITY
CYCLE TIME (SEC): 0.0

```
00001 *      INCREMENTS HIGH TEMP SET-POINT WITH
            ACTIVATION OF UP/DOWN SWITCHES
00002 IF      X3
00003 MATH    V101 := V101 - 1
00004 ENDIF
00005 IF      V101 < 10
00006 MATH    V101 := 10
00007 ENDIF
00008 BINBCD  BINARY INPUT..: V101          BCD RESULT....: V102
00009 IF      X4
00010 MATH    V111 := V111 - 1
00011 ENDIF
00012 IF      V111 < 10
00013 MATH    V111 := 10
00014 ENDIF
00015 BINBCD  BINARY INPUT..: V111          BCD RESULT....: V112
00016 IF      X5
00017 MATH    V121 := V121 - 1
00018 ENDIF
00019 IF      V121 < 10
00020 MATH    V121 := 10
00021 ENDIF
00022 BINBCD  BINARY INPUT..: V121          BCD RESULT....: V122
00023 IF      X6
00024 MATH    V131 := V131 - 1
00025 ENDIF
00026 IF      V131 < 10
00027 MATH    V131 := 10
00028 ENDIF
00029 BINBCD  BINARY INPUT..: V131          BCD RESULT....: V132
**** END ****
```

CONTINUE ON ERROR (Y,N): NO
ERROR STATUS ADDR (Y,C,WY,V): V56 - V58
PROGRAM TYPE (N,P,C,R): PRIORITY
CYCLE TIME (SEC): 0.0

```
00001 *      SETS LOOPS' REMOTE SET-POINTS TO THE
              VALUES CORRESPONDING TO POSITION OF THE
              ROTARY SWITCH
00002 IF      X3
00003 MATH    V210 := V101
00004 ENDIF
00005 IF      X4
00006 MATH    V210 := V111
00007 ENDIF
00008 IF      X5
00009 UNSCALE SCALED INPUT...: V121          BINARY RESULT.: LSP1
              LOW LIMIT.....: 0.0          HIGH LIMIT.....: 100.0
              20% OFFSET.....: NO          BIPOLAR.....: NO
00010 ENDIF
00011 IF      X6
00012 UNSCALE SCALED INPUT...: V131          BINARY RESULT.: LSP1
              LOW LIMIT.....: 0.0          HIGH LIMIT.....: 100.0
              20% OFFSET.....: NO          BIPOLAR.....: NO
00013 ENDIF
**** END ****
```